

Eliminating  $S_1$  between (4-93) and (4-94) yields

$$\dot{e} \left( 1 + \frac{4}{7} e - \frac{4}{21} m \right) = \frac{5}{2} m \left( 1 + \frac{8}{21} e \right) - 2e \left( 1 + \frac{2}{7} e \right) ,$$

which on multiplication by  $(1 - \frac{4}{7} e + \frac{4}{21} m)$  gives the desired boundary (or initial) condition

$$\dot{e} = \frac{5}{2} m - 2e + \frac{4}{7} e^2 - \frac{6}{7} em + \frac{10}{21} m^2 . \quad (4-95)$$

This is the second-order equivalent of (2-118).

As the second boundary condition we may regard the surface flattening  $f = f(1)$  as given. Furthermore, the ellipticity  $e$  must be finite at the earth's center, for  $\beta = 0$ .

### 4.2.3 Radau's Transformation

Following sec. 2.6, we introduce Radau's parameter  $\eta$  by

$$\eta = \frac{\beta}{e} \frac{de}{d\beta} = \frac{\beta}{e} \dot{e} . \quad (4-96)$$

Substituting

$$\dot{e} = \frac{\eta}{\beta} e, \quad \ddot{e} = \left( \frac{1}{\beta} \frac{d\eta}{d\beta} + \frac{\eta^2 - \eta}{\beta^2} \right) e \quad (4-97)$$

(by (2-123)) into (4-91) and dividing by  $e$  gives the second-order Radau equation

$$\beta \frac{d\eta}{d\beta} + \eta^2 - \eta - 6 + 6 \frac{\delta}{D} (1 + \eta) = \frac{4}{7} \left( 1 - \frac{\delta}{D} \right) \xi , \quad (4-98)$$

where (4-92) takes the simpler form

$$\xi = 7\mu(1 + \eta) - 3e(1 + \eta)^2 - 4e \quad (4-99)$$

in view of (4-97). Following the derivation of sec. 2.6 formula by formula, we get (2-134):

$$\frac{d}{d\beta} \left( D\beta^5 \sqrt{1 + \eta} \right) = 5D\beta^4 \psi(\eta) , \quad (4-100)$$

where now

$$\psi(\eta) = (1 + \eta)^{-1/2} \left[ 1 + \frac{1}{2} \eta - \frac{1}{10} \eta^2 + \frac{2}{35} \left( 1 - \frac{\delta}{D} \right) \xi \right] , \quad (4-101)$$

which is (2-132) with a small second-order correction. If  $1 + \lambda_1$  denotes an average value of  $\psi(\eta)$  over the range  $0 \leq \beta \leq 1$ , then the integration of (4-100) gives

$$\int_0^1 D\beta^4 d\beta = \frac{1}{5} \frac{\sqrt{1 + \eta_S}}{1 + \lambda_1} \quad (4-102)$$

since  $D(1) = 1$ .

*Moments of inertia.* The sum of the three principal moments of inertia  $A$ ,  $A$ , and  $C$  is, by (2-138) and (4-14)

$$2A + C = 2 \iiint (x^2 + y^2 + z^2) \rho \, dv = 2 \iiint r^4 \rho \, dr \, d\sigma \quad (4-103)$$

We perform the change of variables discussed in sec. 4.1.2 to get constant limits of integration, using (4-18):

$$2A + C = 2 \iiint r^4 \frac{\partial r}{\partial q} \rho(q) \, dq \, d\sigma \quad (4-104)$$

If we expand  $r$  by (4-50), we immediately see that the first-order terms are removed in view of (2-5), and there remains

$$2A + C = 8\pi \int_0^1 \delta \cdot \beta^4 \, d\beta + O(e^2) \quad (4-105)$$

in our usual new units. This may be written

$$C = \frac{8\pi}{3} \int_0^1 \delta \cdot \beta^4 \, d\beta + \frac{2}{3}(C - A) \quad (4-106)$$

The integral has form (2-141) and may be brought by integration by parts into the form (2-147), so that

$$C = \frac{2}{3}M - \frac{16\pi}{9} \int_0^1 D\beta^4 \, d\beta + \frac{2}{3}(C - A) \quad ; \quad (4-107)$$

note that we are using units in which, so to speak,  $R = 1$  and  $\rho_m = 1$ . In these units the semimajor axis  $a$  is given by (4-46) for  $q = 1$  as

$$a = 1 + \frac{1}{3}e + O(e^2) \quad (4-108)$$

Thus

$$Ma^2 = MR^2 \left(1 + \frac{2}{3}e\right) = \frac{4\pi}{3} \rho_m R^5 \left(1 + \frac{2}{3}e\right) \quad ,$$

which in our units reduces to

$$Ma^2 = \frac{4\pi}{3} \left(1 + \frac{2}{3}e\right) \quad (4-109)$$

Hence the ratio (2-152),

$$\frac{J_2}{H} = \frac{(C - A)/Ma^2}{(C - A)/C} = \frac{C}{Ma^2} = \frac{C}{MR^2} \left(1 - \frac{2}{3}e\right) = \frac{C}{M} \left(1 - \frac{2}{3}e\right) \quad (4-110)$$

becomes, using (4-107),

$$\frac{J_2}{H} = \frac{2}{3} \left(1 - \frac{2}{3}e\right) - \frac{4}{3} \left(1 - \frac{2}{3}e\right) \int_0^1 D\beta^4 d\beta + \frac{2}{3} J_2 + O(e^2) \quad , \quad (4-111)$$

noting that in our units,

$$M = \frac{4}{3} \pi R^3 \rho_m = \frac{4\pi}{3} \quad (4-112)$$

and

$$\frac{C - A}{M} = \frac{C - A}{MR^2} \doteq \frac{C - A}{Ma^2} = J_2 \quad .$$

To the same order we have, by (2-151)

$$J_2 = \frac{2}{3}e - \frac{1}{3}m \quad (4-113)$$

since  $e = f + O(f^2)$ . Thus (4-111) becomes

$$\frac{J_2}{H} = \frac{2}{3} \left[ 1 - \frac{1}{3}m - 2 \left(1 - \frac{2}{3}e\right) \int_0^1 D\beta^4 d\beta \right] \quad , \quad (4-114)$$

from which we eliminate the integral by (4-102).

Hence

$$\frac{J_2}{H} = \frac{2}{3} \left[ 1 - \frac{1}{3}m - \frac{2}{5} \left(1 - \frac{2}{3}e\right) \frac{\sqrt{1 + \eta_S}}{1 + \lambda_1} \right] \quad . \quad (4-115)$$

For  $\eta_S$  we have by (4-95) and (4-96) with  $\beta = 1$ ,

$$1 + \eta_S = \frac{5}{2} \frac{m}{e} - 1 + \frac{4}{7}e - \frac{6}{7}m + \frac{10}{21} \frac{m^2}{e} \quad . \quad (4-116)$$

Eqs. (4-115) and (4-116) provide the extension of (2-153) to second order (Jones, 1954).

#### 4.2.4 Darwin's Equation

It is now not difficult to derive a differential equation for the deviation  $\kappa = \kappa(\beta)$ . We start from the equilibrium condition (4-70) with (4-68). This gives the identity

$$(3e^2 - 8\kappa)D - 6eS + 3P + \frac{8}{3}Q = 0 \quad . \quad (4-117)$$

We eliminate  $S$  by means of (4-88):

$$S = De - \frac{1}{3}D\beta\dot{e} + O(e^2) \quad , \quad (4-118)$$

obtaining

$$(-3e^2 + 2\beta e\dot{e} - 8\kappa)D + 3P + \frac{8}{3}Q = 0 \quad . \quad (4-119)$$